

### 3-5 有熱源的問題

有時候，材料內某些型式的能量會轉變為熱能，如電能、化學能及核能等，此時，可視為內部有熱源。當吾人處理一維、穩態且有熱源的問題時，其統御方程式（熱擴散方程式）為

$$\frac{1}{r^n} \frac{\partial}{\partial r} \left( kr^n \frac{\partial T}{\partial r} \right) + \dot{g} = 0 \quad (3-5.1)$$

其中  $n = \begin{cases} 0 & : \text{直角座標} \\ 1 & : \text{圓柱座標} \\ 2 & : \text{球座標} \end{cases}$

$\dot{g}$  為單位體積的熱源。

若  $k$  為常數，則上式變成

$$\frac{1}{r^n} \frac{\partial}{\partial r} \left( r^n \frac{\partial T}{\partial r} \right) + \frac{\dot{g}}{k} = 0 \quad (3-5.2)$$

吾人以直角及圓柱座標分別討論如下：

#### 1. 平面牆

(3-5.2) 變成

$$\frac{d}{dx} \left( \frac{dT}{dx} \right) + \frac{\dot{g}}{k} = 0$$

積分

$$\frac{dT}{dx} = \int \frac{-\dot{g}}{k} dx$$

再積分

$$T = \int \left( \int \frac{-\dot{g}}{k} dx \right) dx$$

若  $\dot{g}$  為常數，則溫度分布之通解為

$$T = -\frac{\dot{g}}{2k}x^2 + c_1x + c_2 \quad (3-5.3a)$$

將 B.C's 代入，即可求得  $c_1$  與  $c_2$ ，且  $\dot{q}_x$  可得

$$\dot{q}_x = -k \frac{dT}{dx} = \dot{g}x - c_1k \quad (3-5.3b)$$

## 2. 圓柱（管長 $L$ ）

(3-5.2) 變成

$$\begin{aligned} & \frac{1}{r} \frac{d}{dr} \left( r \frac{dT}{dr} \right) + \frac{\dot{g}}{k} = 0 \\ & \Rightarrow \frac{d}{dr} \left( r \frac{dT}{dr} \right) = -\frac{\dot{g}r}{k} \end{aligned}$$

積分

$$\begin{aligned} r \frac{dT}{dr} &= \int \frac{-\dot{g}r}{k} dr \\ &\Rightarrow \frac{dT}{dr} = \frac{1}{r} \int -\frac{\dot{g}r}{k} dr \end{aligned}$$

再積分

$$T = \int \left( \frac{1}{r} \int -\frac{\dot{g}r}{k} dr \right) dr$$

若  $\dot{g}$  為常數，則溫度分布之通解為

$$T = -\frac{\dot{g}r^2}{4k} + c_1 \ln r + c_2 \quad (3-5.4)$$

將 B.C's 代入，即可求得  $c_1$  與  $c_2$ 。對實心圓柱而言，當  $r$  趨近於 0 時， $\ln r$  趨近於  $-\infty$ ，故  $c_1 = 0$ ，上式變成

$$T = -\frac{\dot{q}r^2}{4k} + c_2 \quad (3-5.5a)$$

而  $\dot{q}_r$  及  $\dot{Q}_r$  分別為

$$\dot{q}_r = -k \frac{dT}{dr} = \frac{\dot{q}r}{2} \quad (3-5.5b)$$

$$\dot{Q}_r = \dot{q}_r (2\pi r L) = \dot{q} \pi r^2 L = \dot{q} V_r \quad (3-5.5c)$$

其中  $V_r$  為半徑  $r$  之圓柱體積。



### 例題 3

Consider the plane wall with uniformly distributed heat sources shown in figure. The thickness of the wall in the  $x$  direction is  $2L = 2$  m, A current passing through this conducting material with the heat generated per unit volume is  $\dot{q} = 200$  W/m<sup>3</sup>, and assume the thermal conductivity  $k = 10$  W/m·K does not vary with temperature, the differential equation which governing the heat flow is

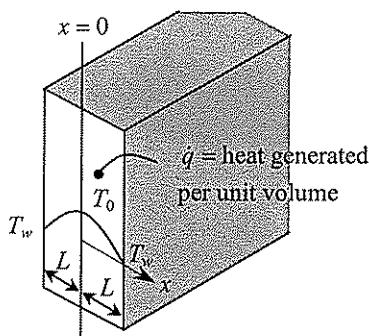
$$\frac{d^2T}{dx^2} + \frac{\dot{q}}{k} = 0$$

For boundary conditions either side of the wall temperature,  $T_w = 30^\circ\text{C}$  at  $x = +L, -L$ .

Determine:

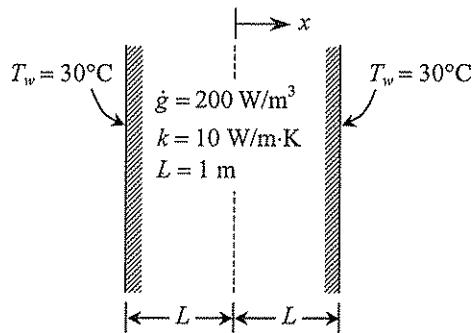
(1) the temperature of the midplane,  $T_0$

(2) the temperature distribution,  $\frac{(T - T_w)}{(T_0 - T_w)}$  (15%)



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解：



由題意可知，熱擴散方程式為

$$\frac{d^2T}{dx^2} + \frac{\dot{g}}{k} = 0$$

積分兩次可得通解為

$$T(x) = -\frac{\dot{g}}{2k} x^2 + c_1 x + c_2$$

而 B.C's 為

$$\begin{cases} T(-L) = T_w \\ T(L) = T_w \end{cases}$$

故  $c_1$  及  $c_2$  分別為

$$c_1 = 0$$

$$c_2 = \frac{\dot{g}L^2}{2k} + T_w$$

因此，溫度分布為

$$T(x) = \frac{\dot{g}L^2}{2k} \left(1 - \frac{x^2}{L^2}\right) + T_w$$

$$(1) \quad T_0 = T(x=0) = \frac{\dot{g}L^2}{2k} + T_w = \frac{200(1)^2}{2(10)} + 30$$

$$= 40 \text{ } (\text{°C})$$

(2) 由上兩式可得

$$\begin{aligned} \frac{T - T_w}{T_0 - T_w} &= \frac{\frac{\dot{g}L^2}{2k} \left(1 - \frac{x^2}{L^2}\right)}{\frac{\dot{g}L^2}{2k}} = 1 - \frac{x^2}{L^2} = 1 - \frac{x^2}{(1)^2} \\ &= 1 - x^2 \end{aligned}$$



#### 例題 4

A plane wall of thickness 0.1 m and thermal conductivity 25 W/(m·K) having uniform volumetric heat generation of 0.3 MW/m<sup>3</sup> is insulated on one side, while the other side is exposed to a fluid at 92°C. The convection heat transfer coefficient between the wall and the fluid is 500 W/(m<sup>2</sup>·K). Determine the maximum temperature in the wall.

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