

【解析】

應變能  $U$  為

$$\begin{aligned}
 U &= 2 \left[ \int_0^{\frac{L}{4}} \frac{(Px)^2}{2EI} dx + \int_{\frac{L}{4}}^{\frac{L}{2}} \frac{\left[ Px - P \left( x - \frac{L}{4} \right) \right]^2}{2EI} dx \right] \\
 &= 2 \left[ \int_0^{\frac{L}{4}} \frac{(Px)^2}{2EI} dx + \int_{\frac{L}{4}}^{\frac{L}{2}} \frac{\left( \frac{PL}{4} \right)^2}{2EI} dx \right]
 \end{aligned}$$

應用卡氏定理如下：

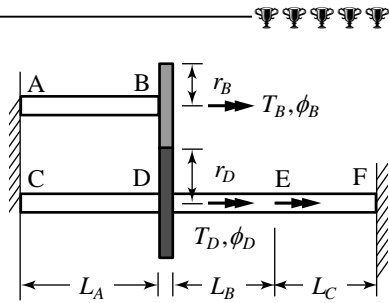
$$\begin{aligned}
 \Delta &= \frac{\partial U}{\partial P} = 2 \left[ \int_0^{\frac{L}{4}} \frac{Px}{EI} \cdot x dx + \int_{\frac{L}{4}}^{\frac{L}{2}} \frac{PL}{4EI} \cdot \frac{L}{4} dx \right] \\
 &= 2 \left[ \frac{P}{EI} \int_0^{\frac{L}{4}} x^2 dx + \frac{PL^2}{16EI} \int_{\frac{L}{4}}^{\frac{L}{2}} dx \right] = 2 \left[ \frac{PL^3}{192EI} + \frac{PL^3}{64EI} \right] = \frac{PL^3}{24EI}
 \end{aligned}$$

所以 A 點之撓度  $\delta_A$  為

$$\delta_A = \frac{\Delta}{2} = \frac{PL^3}{48EI} \quad (\downarrow)$$

• 範題 11 •

Shafts AB and CF as shown in the figure have the same diameter  $d$  and shear modulus  $G$ . A torque  $T_B$  is applied at B. Assume that the torque is transmitted from shaft AB to shaft CF by a single gear-tooth contact force, and neglect the thickness of the gears. It is known that the value of  $r_B/r_D = 1/2$ ,  $T_D = T_E = 0$ ,  $L_A = L_B = L_C = L$ .



- (1) Determine the shaft rotation at E, the rotation of gear D.
- (2) Determine the gear-tooth contact force between gear B and D.

(3) Determine the maximum shear stress in each shaft. (93 交大機械)

此類軸系問題可應用力法或位移法求解，但計算上都相當麻煩，最有效率的解法是應用卡氏第一定理，先將軸系之應變能  $U$  以 B 齒輪之轉角  $\phi_B$  來表示之，則應變能  $U$  對  $\phi_B$  偏微分應等於作用扭矩  $T_B$ ，即可解得  $\phi_B$ ，則齒輪 B 之轉角  $\phi_B$  與齒輪接觸力等均可求得。

【解析】

由齒輪傳動關係知 B 齒輪之轉角  $\phi_B$  與 D 齒輪之轉角  $\phi_D$  具以下關係

$$\frac{\phi_B}{\phi_D} = \frac{r_D}{r_B} = \frac{2}{1} \Rightarrow \phi_D = \frac{1}{2}\phi_B \dots\dots\dots ①$$

因此整個軸系之應變能可以變位表示如下：

$$\begin{aligned} U &= U_{AB} + U_{CD} + U_{DF} \\ &= \frac{GJ\phi_B^2}{2L} + \frac{GJ\phi_D^2}{2L} + \frac{GJ\phi_D^2}{2 \times 2L} = \frac{GJ\phi_B^2}{2L} + \frac{GJ\phi_B^2}{8L} + \frac{GJ\phi_B^2}{16L} \\ &= \frac{11GJ\phi_B^2}{16L} \dots\dots\dots ② \end{aligned}$$

由卡氏第一定理知

$$\frac{\partial U}{\partial \phi_B} = T_B \Rightarrow \frac{11GJ\phi_B}{8L} = T_B \Rightarrow \phi_B = \frac{8T_B L}{11GJ}$$

(1) 軸 E 處之轉角  $\phi_E$  為

$$\phi_E = \frac{1}{2}\phi_D = \frac{1}{4}\phi_B = \frac{2T_B L}{11GJ} \quad \left( \overset{\curvearrowright}{\text{---}} \right)$$

$$\text{齒軸 D 之轉角 } \phi_D = \frac{1}{2}\phi_B = \frac{4T_B L}{11GJ} \quad \left( \overset{\curvearrowright}{\text{---}} \right)$$

(2) 軸 AB 之扭矩  $T_{AB}$  為

$$T_{AB} = \frac{GJ\phi_B}{L} = \frac{8}{11}T_B$$

由齒輪 B 之靜力平衡可得到

$$T_B = T_{AB} + r_B \times F$$

式中  $F$  為齒輪 B 與 D 之接觸力，將  $T_{AB}$  代入上式，可解得

$$F = \frac{3T_B}{11r_B}$$

(3) 軸 CD 所受之扭矩  $T_{CD}$  為

$$T_{CD} = \frac{GJ\phi_D}{L} = \frac{GJ\phi_B}{2L} = \frac{4}{11}T_B$$

而軸 DF 所受之扭矩  $T_{DF}$  為

$$T_{DF} = \frac{GJ\phi_D}{2L} = \frac{GJ\phi_B}{4L} = \frac{2}{11}T_B$$

所以各軸中之最大剪應力如下：

① 軸 AB

$$\tau_{\max} = \frac{T_{AB}r}{J} = \frac{T_{AB} \cdot \frac{d}{2}}{\frac{\pi}{32}d^4} = \frac{16T_{AB}}{\pi d^3} = \frac{128T_B}{11\pi d^3}$$

② 軸 CD

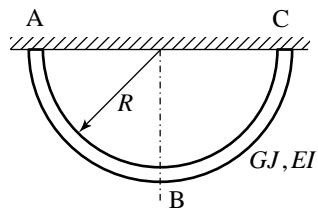
$$\tau_{\max} = \frac{T_{CD}r}{J} = \frac{16T_{CD}}{\pi d^3} = \frac{64T_B}{11\pi d^3}$$

③ 軸 DF

$$\tau_{\max} = \frac{T_{DF}r}{J} = \frac{16T_{DF}}{\pi d^3} = \frac{32T_B}{11\pi d^3}$$

### • 範題 12 •

一細長之半圓形圓環，兩端固定保持在水平面上，如圖所示，當集中負荷  $P$  垂直作用於 B 點時，試求 A 點及 C 點處之反力。



此題題目必須利用對稱性來求解。A 及 C 處之垂直斷面切開後，斷面反力中，應無軸向力，剪力  $V_A = V_C = P/2$ ，彎矩  $M_A = M_C = PR/2$ ，而扭力  $T_A = T_C$ ，但大小未知。再由應變能  $U$  對扭矩  $T_A$  偏微分應等於零，即可解得  $T_A$ 。