

入後，C點端將存在反扭矩  $T_C$  限制C點端轉回去，故相當於  $T_C$  使圓軸轉  $\phi$  角，亦即

$$\frac{T_C \times 5L}{GJ} = \phi = \frac{9t_0 L^2}{2GJ}$$

$$\Rightarrow T_C = \frac{9}{10} t_0 L$$

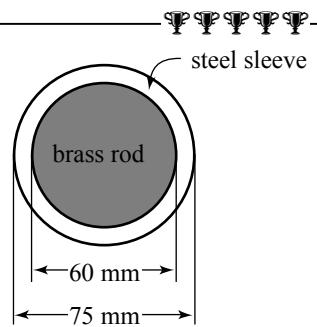
圓軸之殘留應力是因存在反扭矩  $T_C$  而引起，而最大殘留剪應力  $\tau_{\max}$  應發生於圓軸之外表面，其值為

$$\tau_{\max} = \frac{T_C r}{J} = \frac{\frac{9}{10} t_0 L \times \frac{d}{2}}{\frac{\pi \times d^4}{32}} = \frac{72 t_0 L}{5 \pi d^3}$$

### 題型6-8•複合圓軸之靜不定問題

#### •範題 19 •

A composite shaft is formed of two materials, an outer sleeve of steel ( $G_s = 89$  GPa) and an inner rod of brass ( $G_b = 36$  GPa), as shown in figure. The outer diameters of the two parts are 75 mm and 60 mm. Assume that the allowable shear stresses are  $\tau_s = 65$  MPa and  $\tau_b = 25$  MPa in the steel and brass, respectively.



- (1) What is the ratio of the shear stress at the outer diameter of the steel sleeve to the shear stress at the outer diameter of brass rod?
- (2) Which part reaches allowable shear stress first?
- (3) What is the maximum permissible torque  $T$  that may be applied to the shaft?

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## 【解析】

(1)複合圓軸在承受扭矩  $T$  時，其剪應變  $\gamma$  仍沿半徑方向呈線性分布，亦即  $\gamma = \rho\theta$  仍成立，其中  $\rho$  為半徑，而  $\theta$  為單位長度之扭轉角，因此鋼管外徑處之剪應變  $\gamma_s$  與銅桿外徑處之剪應變  $\gamma_b$  之比值應為

$$\frac{\gamma_s}{\gamma_b} = \frac{\frac{75}{2} \times \theta}{\frac{60}{2} \times \theta} = \frac{5}{4}$$

所以鋼管外徑處之剪應力  $\tau_s$  與銅桿外徑處之剪應力之  $\tau_b$  之比值為

$$\frac{\tau_s}{\tau_b} = \frac{G_s \gamma_s}{G_b \gamma_b} = \frac{80 \times 10^9}{36 \times 10^9} \times \frac{5}{4} = 2.78$$

(2)由(1)之結果知鋼管之最大剪應力為銅管最大剪應力之2.78倍，但鋼之容許剪應力  $\tau_s$  只為銅之容許剪應力  $\tau_b$  之  $65/25 = 2.6$  倍，故可知鋼管會先達到容許剪應力。

(3)鋼管之極慣性矩  $J_s$  及銅桿之極慣性矩  $J_b$  分別為

$$J_s = \frac{\pi}{32} \times (75^4 - 60^4) = 1.834 \times 10^6 \text{ mm}^4 = 1.834 \times 10^{-6} \text{ m}^4$$

$$J_b = \frac{\pi}{32} \times 60^4 = 1.272 \times 10^6 \text{ mm}^4 = 1.272 \times 10^{-6} \text{ m}^4$$

當鋼管外徑處剪應力達到容許剪應力時，其所承受之扭矩  $T_s$  可由下式求得：

$$\tau_s = 65 \times 10^6 = \frac{T_s \times \frac{75}{2} \times 10^{-3}}{1.834 \times 10^{-6}}$$

$$\Rightarrow T_s = 3178.93 \text{ N}\cdot\text{m}$$

而此時銅管外徑處之剪應力  $\tau_b$  為

$$\frac{\tau_s}{\tau_b} = 2.78$$

$$\Rightarrow \tau_b = \frac{\tau_s}{2.78} = 23.38 \text{ MPa}$$

故此時圓管所承受之扭矩  $T_b$  為

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$$\tau_b = 23.38 \times 10^6 = \frac{T_b \times \frac{60}{2} \times 10^{-3}}{1.272 \times 10^{-6}}$$

$$\Rightarrow T_b = 991.31 \text{ N}\cdot\text{m}$$

所以複合圓軸之最大容許扭矩  $T_{\max}$  為

$$T_{\max} = T_s + T_b = 3178.93 + 991.31 = 4169.93 \text{ N}\cdot\text{m}$$