

$$F_s = F_c = 36028 \text{ lb}$$

所以螺栓之應力  $\sigma_s$  及鋼管之應力  $\sigma_c$  分別為

$$\sigma_s = \frac{F_s}{A_s} = \frac{36028}{\frac{1}{2}}$$

$$= 72.056 \text{ ksi}$$

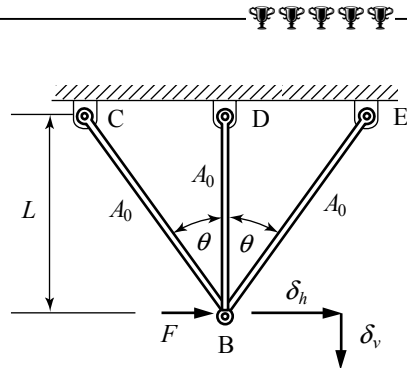
$$\sigma_c = \frac{F_c}{A_c} = \frac{36028}{\frac{3}{4}}$$

$$= 48.037 \text{ ksi}$$

### 題型4-8 左右不對稱之一般靜不定結構

#### 範題 13

Consider the pin-connected truss as shown in Fig. The three bars have the same cross-sectional area  $A_0$  and Young's modulus  $E$ . A horizontal force  $F$  is applied to joint B.

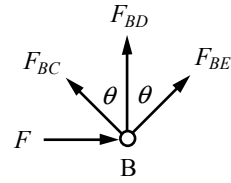


- (1) Is the structure statically determinate or statically indeterminate?
- (2) Draw the free-body diagram of joint B and write down the equilibrium equations.
- (3) Let  $\delta_h$  and  $\delta_v$  indicate the horizontal and vertical displacements of joint B, respectively. Express the change in length of each bar in terms of  $\delta_h$  and  $\delta_v$ .
- (4) If the three bars have the same allowable load  $F_{\text{allow}}$ , determine the largest value of the horizontal force  $F$ .

(90台大機械)

【解析】

(1) 因為有三根桿件，故有三個未知軸力，若取點B為分離體，則只能列出兩個獨立方程式，所以結構為一維靜不定。



(2) 分別考慮水平方向及垂直方向之靜力平衡，可列出

$$+F - F_{BC} \sin \theta + F_{BE} \sin \theta = 0 \dots\dots\dots ①$$

$$+F_{BC} \cos \theta + F_{BD} + F_{BE} \cos \theta = 0 \dots\dots\dots ②$$

式中  $F_{BC}$ 、 $F_{BD}$  及  $F_{BE}$  分別為桿 BC、BD 及 BE 之受力。

(3) 點B 水平變位  $\delta_h$  引起各桿之變形量如下：

$$\delta_{BC} = \delta_h \sin \theta$$

$$\delta_{BD} = 0$$

$$\delta_{BE} = -\delta_h \sin \theta$$

點B 垂直變位  $\delta_v$  引起各桿之變形量如下：

$$\delta_{BC} = \delta_v \cos \theta$$

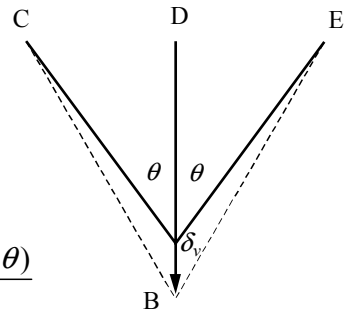
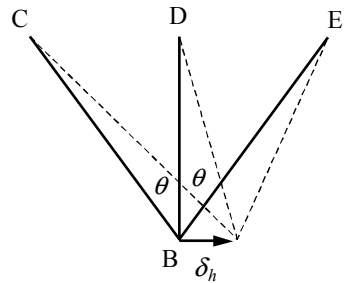
$$\delta_{BD} = \delta_v$$

$$\delta_{BE} = \delta_v \cos \theta$$

所以點B 水平變位  $\delta_h$  與垂直變位  $\delta_v$  所

引起之各桿之變形量如下：

$$\begin{cases} \delta_{BC} = +\delta_h \sin \theta + \delta_v \cos \theta \\ \delta_{BD} = 0 + \delta_v = \delta_v \\ \delta_{BE} = -\delta_h \sin \theta + \delta_v \cos \theta \end{cases} \dots\dots\dots ③$$



(4) 由式③及變形量公式可得到

$$\delta_{BC} = +\delta_h \sin \theta + \delta_v \cos \theta = \frac{F_{BC}(L/\cos \theta)}{A_0 E}$$

$$\Rightarrow F_{BC} = \frac{A_0 E}{L} (\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \dots\dots\dots ④$$

$$\delta_{BD} = 0 + \delta_v = \delta_v = \frac{F_{BD} L}{A_0 E}$$

$$\Rightarrow F_{BD} = \frac{\delta_v A_0 E}{L} \dots\dots\dots ⑤$$

$$\begin{aligned} \delta_{BE} &= -\delta_h \sin \theta + \delta_v \cos \theta \\ &= \frac{F_{BE}(L/\cos \theta)}{A_0 E} \end{aligned}$$

$$\Rightarrow F_{BE} = \frac{A_0 E}{L} (-\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \dots\dots\dots ⑥$$

將式④、⑤及⑥代入式①及②，可得到

$$\begin{aligned} +F - \frac{A_0 E}{L} (\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \sin \theta \\ + \frac{A_0 E}{L} (-\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \sin \theta = 0 \dots\dots\dots ⑦ \end{aligned}$$

$$\begin{aligned} \frac{A_0 E}{L} (\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \cos \theta + \frac{\delta_v A_0 E}{L} \\ + \frac{A_0 E}{L} (-\delta_h \sin \theta \cos \theta + \delta_v \cos^2 \theta) \cos \theta = 0 \dots\dots\dots ⑧ \end{aligned}$$

由式⑧可求得  $\delta_v = 0$ ，代入式⑦中，可解出  $\delta_h$  為

$$\delta_h = \frac{FL}{2A_0 E \sin^2 \theta \cos \theta} \dots\dots\dots ⑨$$

再代入式④、⑤及⑥，即可求出

$$F_{BC} = \frac{F}{2 \sin \theta}$$

$$F_{BD} = 0$$

$$F_{BE} = -\frac{F}{2 \sin \theta}$$

又因為桿件所能承受之容許負載為  $F_{\text{allow}}$ ，故

$$F_{BC} = \frac{F}{2 \sin \theta} \leq F_{\text{allow}}$$

$$\Rightarrow F \leq 2F_{\text{allow}} \sin \theta$$

所以結構所能承受之最大作用力  $F = 2F_{\text{allow}} \sin \theta$ 。